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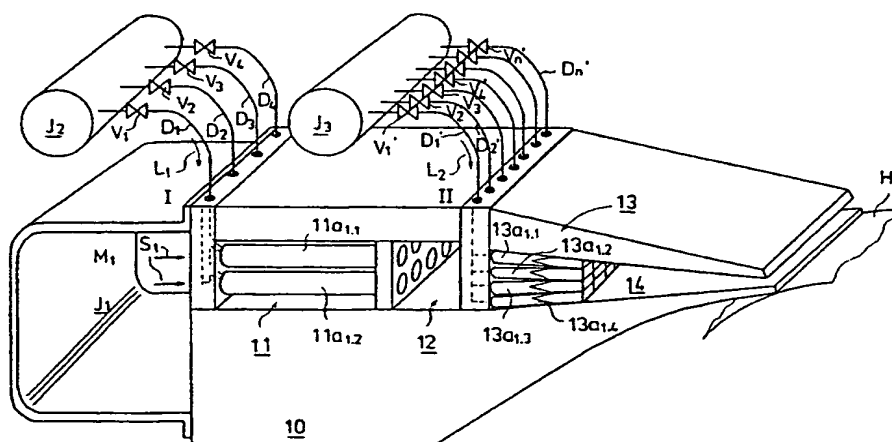
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With amended claims.

In English translation (filed in Finnish).

(54) Title: METHOD AND APPARATUS FOR MIXING DILUTION LIQUID INTO A STOCK FLOW IN A PAPER OR BOARD MACHINE



## (57) Abstract

The invention relates to a method and an apparatus for mixing dilution liquid into a stock flow in a paper or board machine. In the method, dilution is carried out in at least two stages using in the first dilution stage (I) valves ( $V_1, V_2, V_3, \dots$ ) fitted with a larger mutual spacing at different points of width across a headbox and passing the dilution water through said valves to desired points of width of the headbox according to the requirement of control of the basis weight of paper or board. In the method, in the second dilution stage (II), dilution water is passed into connection with the stock flow coming from the first dilution stage (I), said dilution water being controlled by means of valves ( $V_1', V_2', \dots$ ), which valves ( $V_1', V_2', \dots$ ) have been fitted with a denser spacing than the valves ( $V_1, V_2, V_3, \dots$ ) of the first dilution stage (I).

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Method and apparatus for mixing dilution liquid  
into a stock flow in a paper or board machine

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The invention relates to a method and an apparatus for mixing dilution liquid into a stock flow in a paper or board machine.

10 With respect to the prior art, we refer to the publications DE 19723861 and FI 901593.

It has become clear that with the development of measuring devices on the market ever higher requirements are set for the accuracy of control of the basis weight  
15 profile. Today, the dilution spacing in a so-called dilution headbox is about 32-75 mm, and it is not possible to reduce it any more if fibre-containing white water is used as dilution water, because dilution feed ducts which remain open by means of white water cannot be accommodated between tube rows with a dense spacing.

20 As a solution it is proposed that, when needed, dilution is changed to comprise two stages such that coarse control is carried out by means of white water and fine control is carried out by means of raw water.

The increasing requirement of control accuracy calls for an increasingly denser  
25 dilution spacing and, therefore, still narrower dilution feed ducts. If white water is used as dilution water, narrow dilution ducts clog easily. Clogging problems are not encountered with raw water, but its "full-scale use" is not economical and sensible for environmental reasons.

30 The idea of the two-stage dilution is to correct large basis weight profile errors by a large amount of white water and small profile errors by a small amount of raw water. A good raw water economy is achieved by this means in a paper mill.

Another benefit of the two-stage arrangement is the good possibility of adjusting the basis weight profile. The entire valve control area can be made use of and control valves of an optimum size can be selected for both control operations.

- 5 Coarse control is carried out in a tube bank after an inlet header, as in the conventional headbox. In the first dilution stage, the control spacing can be increased, for example, to 120 mm such that one dilution member feeds two tube rows. Course control corrects major errors in the shape of the profile, such as, for example, profile errors arising from web shrinkage. The small errors which remain in the  
10 profile after coarse control are rectified by means of fine control dilution in the second stage.

- Fine adjustment is carried out as turbulence generator dilution by supplying some or each of the tubes of the turbulence generator with dilution liquid. A very small  
15 amount of dilution liquid is needed for rectifying the remaining small errors, so raw water or clarified white water obtained from a fibre recovery unit can be used economically as dilution water in fine control. Since, for example, raw water does not contain contaminating or clogging particles, the dilution ducts can be provided in very narrow spaces. Moreover, the control valves and the actuators operating the  
20 valves can be ordinary standard devices available on the market, which devices are considerably less expensive than conventional dilution valves and actuators.

- Minimum local dilution with raw water can be almost 0 % and maximum local dilution need not be high because the consistency of raw water is 0 % and the  
25 remaining error to be corrected is small. Thus, the amount of the more expensive raw water consumed is very small. No separate circulation is required for the feed of raw water.

- The price of the arrangement disclosed hardly differs at all from the price of the  
30 conventional dilution headbox. The proposed arrangement uses half the number of expensive dilution valves and actuators.

Thus, mixing units are prior known in which dilution water and stock passed from the inlet header of the headbox are mixed and the combined flow is passed further onwards in the headbox and onto a forming wire. Points of supply of dilution liquid are situated in different positions of width across the headbox and, thus, depending on the density of the dilution points placed across the width of the headbox, desired resolution is obtained for control of the basis weight of the web.

The method and the apparatus according to the invention are characterized in what is set forth in the claims.

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Thus, this application proposes using dilution in at least two stages. Coarse control of the basis weight profile is carried out in the first stage of dilution and fine control is carried out in the second stage of dilution. White water is used as dilution water in the first stage and the valves are arranged with a less dense spacing in the first stage than in the second control stage in which the valves are arranged with a denser spacing than in the first dilution stage. An advantage of the arrangement is that the valves of the second stage can have a construction that demands less precision and thus be less expensive than the valves of the first stage. They do not clog because fibre-free dilution water is used in the second stage. The valves can thus contain smaller ducts. They do not demand much space.

20

Within the scope of the invention, it is also possible to use control with three or more stages, but the most advantageous control arrangement is two-stage adjustment of the dilution liquid.

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The headbox structure of the paper or board machine can advantageously be as follows:

- a) stock is passed into a stock inlet header which tapers towards its outlet end in a conventional manner.
- b) the stock flow is passed from the stock inlet header into a tube bank and further through the tube bank into an intermediate chamber.

30

- c) the stock flow is passed from the intermediate chamber further into a turbulence generator and from the turbulence generator further through a slice cone onto a forming wire.

5 In the following, the invention will be described with reference to some advantageous embodiments of the invention shown in the figures of the accompanying drawings, to which the invention is, however, not intended to be exclusively confined.

10 In accordance with the invention, the valves of the first dilution stage are located in connection with the tube bank and the valves of the second dilution stage are located after the intermediate chamber in connection with the turbulence generator.

15 Figures 1A—1C show the method according to the invention in stages. The graph  $F_1$  in Fig. 1A represents an uncorrected basis weight profile of stock passed from an inlet header  $J_1$  across the width of the machine. In the first dilution stage, coarse control of the basis weight profile is carried out by means of valves  $V_1, V_2, \dots$  of the first dilution stage.

20 The graph  $F_1'$  in Fig. 1B shows a basis weight profile after the valves  $V_1, V_2, \dots$  controlling the basis weight profile.

25 In Fig. 1C, the graph  $F_2$  shows a corrected basis weight profile of stock after the second dilution stage. Dilution valves  $V_1', V_2', \dots$  of the second dilution stage are placed, for example, in connection with a turbulence generator. The graph  $F_2$  shows the basis weight profile in the stock flow across the width of the machine after adjustment carried out by the valves  $V_1', V_2', \dots$  of the second stage.

30 In Figs. 1A—1C, the horizontal coordinate  $X$  represents headbox operation and the vertical coordinate  $Y$  represents the basis weight. A basis weight deviation from the zero level, i.e. a basis weight error, occurring in the stock and further in the web can be read from the vertical coordinate  $Y$ . The basis weight profile can be

measured from the stock flow, but the easiest way to measure the basis weight is to measure it from a finished paper or board web.

Figure 2 shows a headbox of a paper or board machine in accordance with the invention.

In Fig. 1A, the first graph  $F_1$  shows control in the first dilution stage. The graph  $F_1$  depicts a basis weight variation which occurs in the stock before the control valves  $V_1, V_2, V_3 \dots$  of the first stage.

In Fig. 1A, the graph  $F_1$  shows a basis weight variation which occurs in the stock  $M_1$ . An average basis weight variation is further shown by the graph  $F_{10}$ . As seen in the graph  $F_{10}$ , in the basis weight there is firstly a shape error and secondly a local error. Said shape error is corrected by means of the control valves  $V_1, V_2 \dots$  of the first dilution stage I such that the graph  $F_{10}$  becomes straight. The local errors are rectified by means of the control valves  $V_1', V_2' \dots$  in the basis weight adjustment of the second stage II.

The graph  $F_1'$  of Fig. 1B illustrates the situation after the first stage, in which connection control of the basis weight of the stock  $M_1$  has been accomplished by introduction of dilution liquid. In the graph, the horizontal coordinate X represents the cross-direction position of the headbox and the positions of the valves are denoted with  $V_1', V_2', V_3' \dots$  in the horizontal coordinate X. The vertical coordinate Y shows a basis weight error of the stock after the adjustment of the first stage I.

Fig. 1C shows the basis weight control of the second dilution stage II. The graph  $F_2$  illustrates the situation after the dilution liquid valves  $V_1', V_2', V_3' \dots$  of the second dilution stage. The graph  $F_2$  is straight and there does not occur any basis weight error any more. In the graph, the horizontal coordinates represent the width of the headbox, and the position of the valves is denoted with  $V_1', V_2' \dots$  at each particular point of the horizontal coordinate X. The vertical coordinate Y shows the basis weight error of the stock. The zero level illustrates a correct constant basis weight

situation. White water is used as dilution water in the first stage I, which water may contain fibres and fines/fillers. The dilution of the second stage II is carried out by means of dilution water which does not contain fibres, such as raw water. A benefit in that case is that conventional valves  $V_1'$ ,  $V_2'$ ,  $V_3'$ ... can be used because there is  
5 no risk of the ducts being clogged by fibres.

The dilution water feeds of the kind mentioned can be placed with a denser spacing than those of the current arrangements, the spacing between the valves in dilution control can be reduced from 60 mm to 30 mm. The amount of the dilution water  
10 used is small and there is no need for a separate circulation of the dilution water. Consequently, the construction of the arrangement according to the invention is advantageous and it allows a denser spacing to be used between the valves, i.e. higher resolution, i.e. a higher accuracy of control. By using raw water in the adjustment of the second stage it is possible to employ conventional valve arrange-  
15 ments, in which connection the valves can also be placed with a spacing of even 20-30 mm with respect to one another, whereas in the adjustment of the first stage, the control resolution can be changed in the case of said stage so that the valves are disposed, for example, with a spacing of 120 mm with respect to one another instead of, for example, conventional single-stage dilution of 60 mm. Thus, by using the  
20 arrangement in accordance with the invention in which the dilution of the first stage employs white water as dilution water and the dilution of the second stage employs fibre-free dilution water, an overall end result is achieved in which the accuracy of control is better than in conventional single-stage dilution and in which the construction costs with respect to structure have, however, not increased as compared with  
25 single-stage dilution.

The coarse control of the basis weight profile is carried out in the first stage of dilution and the fine control thereof is carried out in the second stage of dilution. The dilution water used in the second dilution stage is advantageously raw water or  
30 clarified white water. Thus, the dilution water of the second stage contains solids and/or fibres substantially less in percentage terms than the dilution water of the first stage, which is advantageously water taken out of the wire. Most advantageously,



the dilution water of the second stage is raw water that does not contain any solids and fillers and fibres.

- Fig. 2 shows a headbox 10 of a paper or board machine in accordance with the invention. The headbox comprises a stock inlet header  $J_1$ , a tube bank 11 after the stock inlet header, an intermediate chamber 12 after the tube bank, and a turbulence generator 13 after the intermediate chamber, and further a slice cone 14 from which stock  $M_1$  is passed onto a forming wire  $H_1$ . In accordance with the invention, dilution of the first stage is carried out in tubes  $11a_{1.1}, 11a_{1.2}, 11a_{4.1}, 11a_{4.2} \dots$  of the tube bank 11 through valves  $V_1, V_2, V_3 \dots$ . White water is passed from a white water inlet header  $J_2$  (arrow  $L_1$ ) into tubes  $D_1, D_2, D_3 \dots$  and through them into the valves  $V_1, V_2, V_3 \dots$  and further through said adjustable valves  $V_1, V_2 \dots$  into the tubes  $11a_{1.1}, 11a_{1.2}, 11a_{4.1}, 11a_{4.2} \dots$  of the tube bank 11. The valves  $V_1, V_2, V_3 \dots$  are located, for example, with a spacing of 120 mm in connection with the headbox having a width of 10 m. The second dilution location, i.e. valves  $V_1', V_2' \dots$  of the second dilution stage II are advantageously located in connection with turbulence pipes  $13a_{1.1}, 13a_{1.2}, 13a_{1.3}, 13a_{2.1}, 13a_{2.2}, 13a_{2.3}$  of the turbulence generator 13 at different points of width across the headbox. Raw water is passed (arrow  $L_2$ ) from a raw water inlet header  $J_3$  into a duct  $D_1', D_2', D_3' \dots$  and through the valves  $V_1', V_2' \dots$  further into the pipes  $13a_{1.1}, 13a_{1.2}, 13a_{1.3}, 13a_{2.1}, 13a_{2.2}, 13a_{2.3}$  of the turbulence generator 13, in which the raw water is passed into connection with the stock diluted in the first stage. The flow of the stock  $M_1$  is denoted with the arrows  $S_1$  and the flow of the dilution waters is denoted with the arrows  $L_1$  and  $L_2$ .
- When the dilution liquid is passed into connection with the stock flow in the first dilution stage and in the second stage, the dilution water is passed in the first dilution stage I either into one or more, advantageously all tubes of the tube row of the tube bank 11 at the width point in question. Similarly, in the second dilution stage II, the dilution water can be passed either into one tube of the turbulence generator 13 at the width point in question or into more tubes, advantageously into all tubes at the width point in question.

## Claims

1. A method for passing dilution water into connection with a stock flow passed from a stock inlet header of a headbox in a paper or board machine, **characterized** in that, in the method, dilution is carried out in at least two stages using in the first dilution stage (I) valves ( $V_1, V_2, V_3 \dots$ ) fitted with a larger mutual spacing at different points of width across the headbox and passing the dilution water through said valves to desired points of width of the headbox according to the requirement of control of the basis weight of paper or board, and that, in the method, in the second dilution stage (II), dilution water is passed into connection with the stock flow coming from the first dilution stage (I), said dilution water being controlled by means of valves ( $V_1', V_2' \dots$ ), which valves ( $V_1', V_2' \dots$ ) have been fitted with a denser spacing than the valves ( $V_1, V_2, V_3 \dots$ ) of the first dilution stage (I).
2. A method according to claim 1, **characterized** in that coarse control of the basis weight profile of the stock ( $M_1$ ) is carried out in the first stage (I) of dilution and fine control of the basis weight profile of the stock ( $M_1$ ) is carried out in the second stage (II) of dilution.
3. A method according to claim 1 or 2, **characterized** in that in the second stage (II) of dilution, as dilution water is used water the solids, filler or fibre content of which is substantially lower in percentage terms than that of the dilution water of the first stage (I) of dilution.
4. A method according to any one of the preceding claims 1 to 3, **characterized** in that the dilution water used in the second dilution stage (II) is raw water or clarified white water.
5. A method according to any one of the preceding claims, **characterized** in that the dilution water of the first stage (I) is white water.

6. A headbox (10) of a paper or board machine which comprises a stock inlet header ( $J_1$ ) and after that a tube bank (11) and after the tube bank an intermediate chamber (12) and after the intermediate chamber a turbulence generator (13) and after the turbulence generator a slice cone (14) from which stock is passed further  
5 onto a forming wire ( $H_1$ ), characterized in that the apparatus comprises valves ( $V_1, V_2, V_3, \dots$ ) of a first dilution stage (I), through which valves dilution water is passed into connection with the stock ( $M_1$ ) passed from the inlet header ( $J_1$ ) to desired points across the width of the headbox so as to control the basis weight of the web in the first stage (I), and that the headbox comprises valves ( $V_1', V_2', V_3', \dots$ ) of a  
10 second dilution stage (II), through which valves ( $V_1', V_2', \dots$ ) the dilution water of the second stage is passed into connection with the stock ( $M_1$ ) coming from the first dilution stage (I).

7. A headbox of a paper or board machine according to claim 6, characterized in  
15 that the dilution water of the first dilution stage (I) is passed into connection with the stock ( $M_1$ ) passed from the stock inlet header ( $J_1$ ) in connection with the tube bank (11), and that the dilution water of the second dilution stage (II) is passed into connection with the stock ( $M_1$ ) coming from the first dilution stage (I) in connection with the turbulence generator (13).

8. A headbox according to claim 6 or 7, characterized in that the valves ( $V_1, V_2, V_3, \dots$ ) of the first dilution stage (I) are spaced a longer distance from one another than the valves ( $V_1', V_2', V_3', \dots$ ) of the second dilution stage (II), in which connection coarse control of the basis weight of the web is carried out by means of the  
25 valves ( $V_1, V_2, \dots$ ) of the first dilution stage (I) and fine control of the basis weight of the web is carried out by means of the valves ( $V_1', V_2', \dots$ ) of the second dilution stage (II).

9. A headbox according to any one of the preceding claims 6 to 8, characterized  
30 in that the apparatus comprises an inlet header ( $J_3$ ) for the dilution water of the second dilution stage (II), said inlet header comprising raw water as dilution water.

**AMENDED CLAIMS**

[received by the International Bureau on 14 September 2000 (14.09.00);  
original claims 1-9 replaced by new claims 1-7 (2 pages)]

1. A method for passing dilution water into connection with a stock flow passed from a stock inlet header of a headbox in a paper or board machine, **characterized** in that, in  
5 the method, dilution is carried out in at least two stages using in the first dilution stage (I) valves ( $V_1, V_2, V_3, \dots$ ) fitted with a larger mutual spacing at different points of width across the headbox and passing the dilution water through said valves to desired points of width of the headbox according to the requirement of control of the basis weight of paper or board, and that, in the method, in the second dilution stage (II), dilution water  
10 is passed into connection with the stock flow coming from the first dilution stage (I), said dilution water being controlled by means of valves ( $V'_1, V'_2, \dots$ ), which valves ( $V'_1, V'_2, \dots$ ) have been fitted with a denser spacing than the valves ( $V_1, V_2, V_3, \dots$ ) of the first dilution stage (I), and that coarse control of the basis weight profile of the stock ( $M_1$ ) is carried out in the first dilution stage (I) and fine control of the basis weight profile of the  
15 stock ( $M_1$ ) is carried out in the second dilution stage (II) across the width of the machine.

2. A method according to claim 1, **characterized** in that in the second stage (II) of dilution, as dilution water is used water the solids, filler or fibre content of which is  
20 substantially lower in percentage terms than that of the dilution water of the first stage (I) of dilution.

3. A method according to claim 1 or 2, **characterized** in that the dilution water used in the second dilution stage (II) is raw water or clarified white water.

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4. A method according to any one of the preceding claims, **characterized** in that the dilution water of the first stage (I) is white water.

5. A headbox (10) of a paper or board machine which comprises a stock inlet header  
30 ( $J_1$ ) and after that a tube bank (11) and after the tube bank an intermediate chamber (12) and after the intermediate chamber a turbulence generator (13) and after the turbulence

- generator a slice cone (14) from which stock is passed further onto a forming wire ( $H_1$ ), characterized in that the apparatus comprises valves ( $V_1, V_2, V_3, \dots$ ) of a first dilution stage (I), through which valves dilution water is passed into connection with the stock ( $M_1$ ) passed from the inlet header ( $J_1$ ) to desired points across the width of the headbox
- 5 so as to control the basis weight of the web in the first stage (I), and that the headbox comprises valves ( $V_1', V_2', V_3', \dots$ ) of a second dilution stage (II), through which valves ( $V_1', V_2', \dots$ ) the dilution water of the second stage is passed into connection with the stock ( $M_1$ ) coming from the first dilution stage (I), and that the valves ( $V_1, V_2, V_3, \dots$ ) of the first dilution stage (I) are spaced a longer distance from one another than the valves
- 10 ( $V_1', V_2', V_3', \dots$ ) of the second dilution stage (II), in which connection coarse control of the basis weight of the web is carried out by means of the valves ( $V_1, V_2, \dots$ ) of the first dilution stage (I) and fine control of the basis weight of the web is carried out by means of the valves ( $V_1', V_2', \dots$ ) of the second dilution stage (II).
- 15 6. A headbox of a paper or board machine according to claim 5, characterized in that the dilution water of the first dilution stage (I) is passed into connection with the stock ( $M_1$ ) passed from the stock inlet header ( $J_1$ ) in connection with the tube bank (11), and that the dilution water of the second dilution stage (II) is passed into connection with the stock ( $M_1$ ) coming from the first dilution stage (I) in connection with the turbulence
- 20 generator (13).
7. A headbox according to claim 5 or 6, characterized in that the apparatus comprises an inlet header ( $J_2$ ) for the dilution water of the second dilution stage (II), said inlet header comprising raw water as dilution water.

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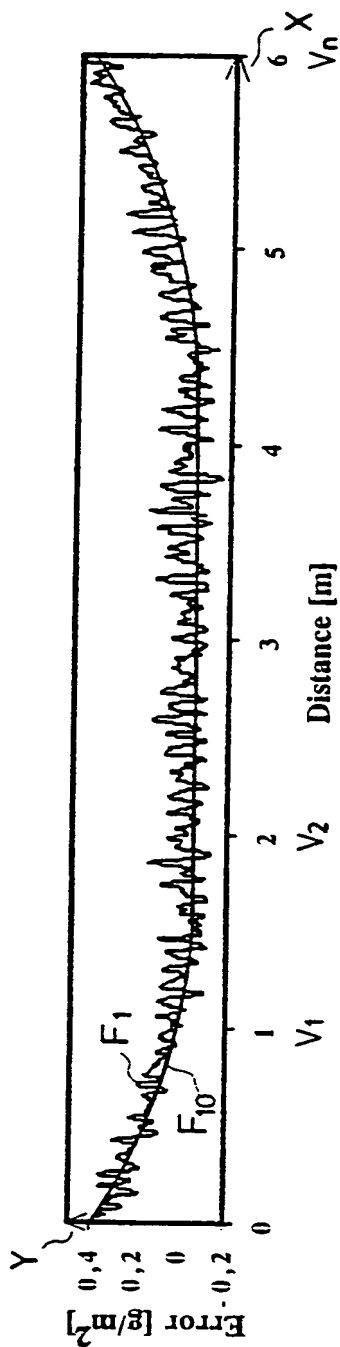


FIG. 1A

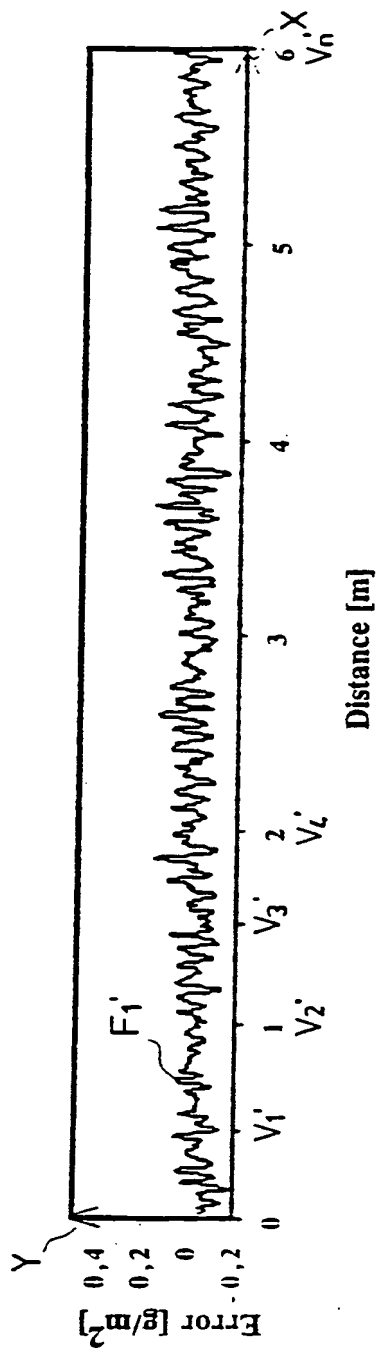


FIG. 1B

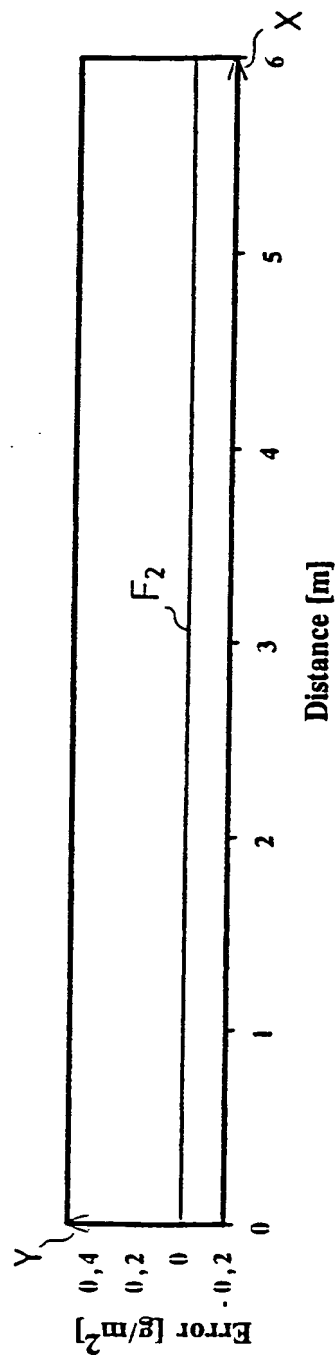


FIG. 1C





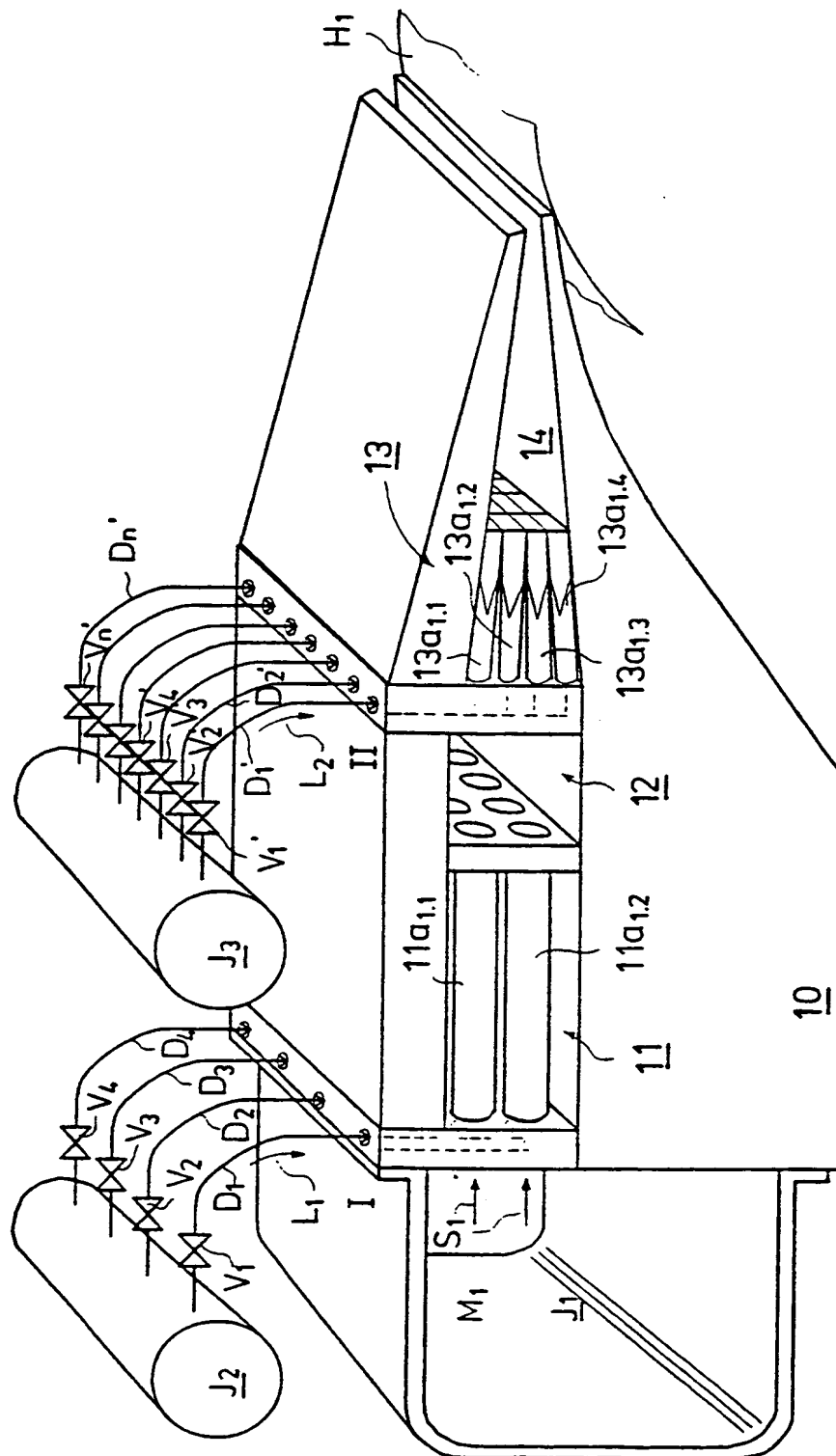


FIG. 2



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1  
INTERNATIONAL SEARCH REPORT

International application No.

PCT/FI 00/00320

## A. CLASSIFICATION OF SUBJECT MATTER

IPC7: D21F 1/02, D21F 1/08

According to International Patent Classification (IPC) or to both national classification and IPC

## B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

IPC7: D21F

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

SE,DK,FI,NO classes as above

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

## C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	EP 0824157 A2 (VOITH SULZER PAPIERMASCHINEN GMBH), 18 February 1998 (18.02.98), column 8, line 22 - column 11, line 21, figures 1-4  --	1-9
X	US 4897158 A (ELMER WEISSHUHN ET AL), 30 January 1990 (30.01.90), column 12, line 10 - column 13, line 58, figure 6  -----	1-9

☐ Further documents are listed in the continuation of Box C.☒ See patent family annex.

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Information on patent family members

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